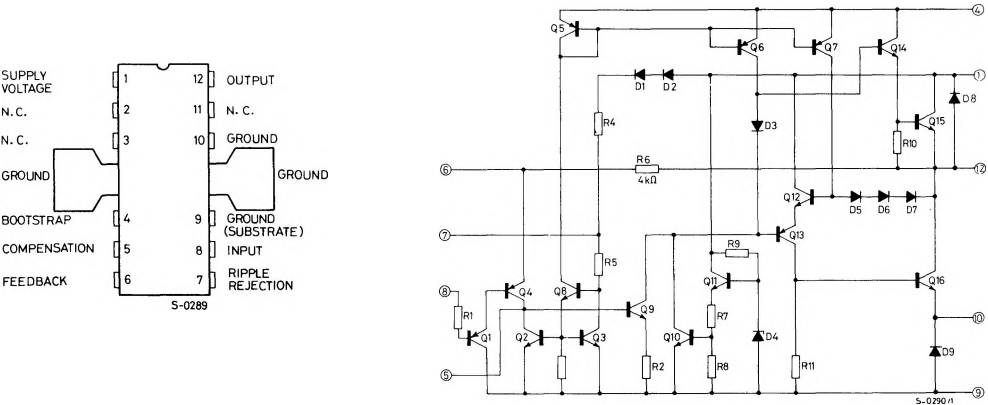




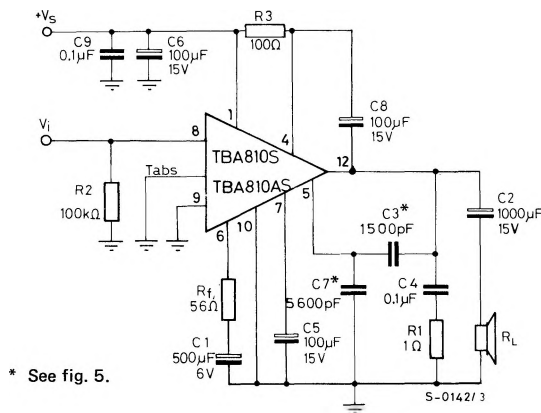
TBA 810 AS



CONNECTION AND SCHEMATIC DIAGRAM (top view)



TEST AND APPLICATION CIRCUIT



THERMAL DATA			TBA810S	TBA810AS
$R_{th \text{ j-tab}}$	Thermal resistance junction-tab	max	12 °C/W	10 °C/W
$R_{th \text{ j-amb}}$	Thermal resistance junction-ambient	max	70 °C/W	80 °C/W

* Obtained with tabs soldered to printed circuit with minimized copper area.

ELECTRICAL CHARACTERISTICS (Refer to the test circuit; $T_{amb} = 25^{\circ}C$)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage (pin 1)		4		20	V
V_o Quiescent output voltage (pin 12)	$V_s = 14.4V$	6.4	7.2	8	V
I_d Quiescent drain current			12	20	mA
I_b Bias current (pin 8)			0.4		μA
P_o Power output	$d = 10\%$ $R_L = 4\Omega$ $f = 1\text{ kHz}$ $V_s = 16V$ $V_s = 14.4V$ $V_s = 9V$ $V_s = 6V$	5.5	7 6 2.5 1		W W W W
$V_{i(rms)}$ Input voltage				220	mV
V_i Input sensitivity	$P_o = 6W$ $V_s = 14.4V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$ $R_f = 56\Omega$ $R_f = 22\Omega$		80 35		mV mV
R_i Input resistance (pin 8)			5		M Ω
B Frequency response (-3 dB)	$V_s = 14.4V$ $R_L = 4\Omega$ $C3 = 820\text{ pF}$ $C3 = 1500\text{ pF}$		40 to 20,000 40 to 10,000		Hz Hz
d Distorsion	$P_o = 50\text{mW to } 3W$ $V_s = 14.4V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$		0.3		%
G_v Voltage gain (open loop)	$V_s = 14.4V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$		80		dB
G_v Voltage gain (closed loop)	$V_s = 14.4V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$	34	37	40	dB
e_N Input noise voltage	$V_s = 14.4V$ $R_g = 0$ $B (-3\text{ dB}) = 20\text{ Hz to } 20,000\text{ Hz}$		2		μV
i_N Input noise current	$V_s = 14.4V$ $B (-3\text{ dB}) = 20\text{ Hz to } 20,000\text{ Hz}$		0.1		nA
η Efficiency	$P_o = 5W$ $V_s = 14.4V$ $R_L = 4\Omega$ $f = 1\text{ kHz}$		70		%
SVR Supply voltage rejection	$V_s = 14.4V$ $R_L = 4\Omega$ $f_{ripple} = 100\text{ Hz}$		38		dB



TBA810S

Fig. 1 - Power output versus supply voltage

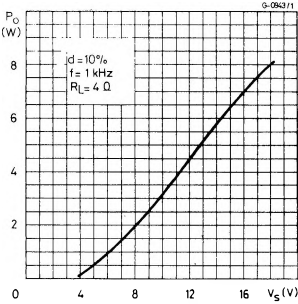


Fig. 2 - Maximum power dissipation versus supply voltage (sine wave operation)

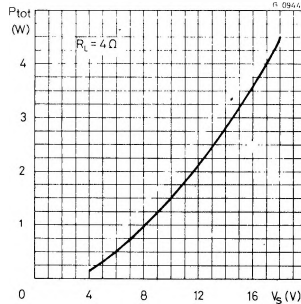


Fig. 3 - Distorsion versus output power

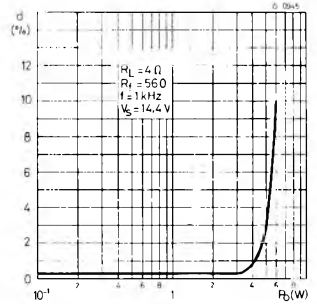


Fig. 4 - Distorsion versus frequency

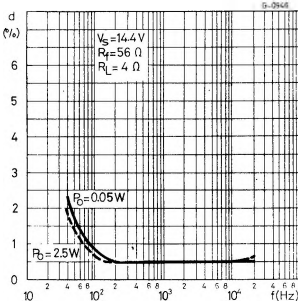


Fig. 5 - Value of C3 versus RL for various values of B

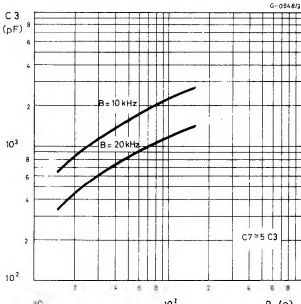


Fig. 6 - Power dissipation and efficiency versus output power

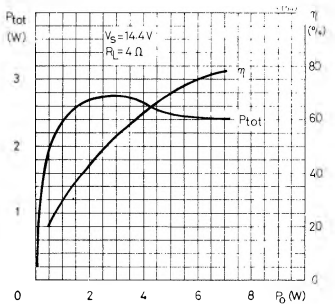


Fig. 7 - Quiescent output voltage (pin 12) versus supply voltage

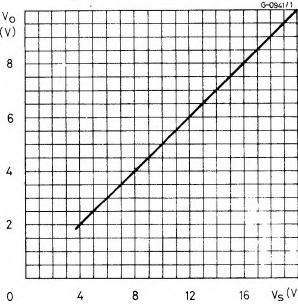


Fig. 8 - Quiescent current versus supply voltage

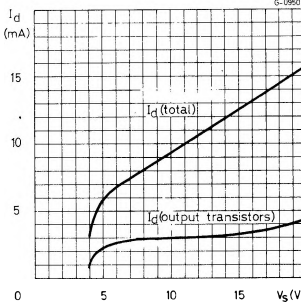
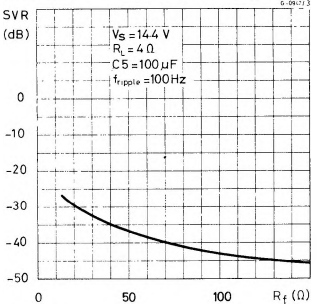


Fig. 9 - Supply voltage rejection

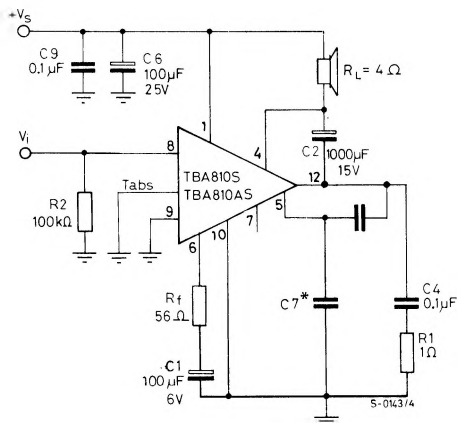


SSS

TBA810S

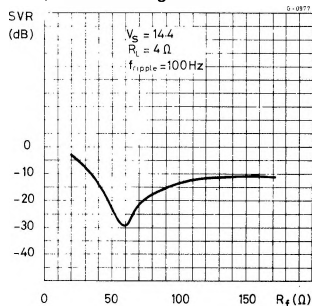
For portable equipment the circuit in Fig. 10 has the advantages of fewer external components and a better behaviour at low supply voltages (down to 4 V).

Fig. 10 - Application circuit with load connected to the supply voltage



* C3, C7 see fig. 5

Fig. 11 - Supply voltage rejection versus R_f (circuit of fig. 10)



MOUNTING INSTRUCTIONS

The thermal power dissipated in the circuit may be removed by connecting the tabs to an external heat sink (TBA 810 AS - fig. 12) or by soldering them to an area of copper on the printed circuit board (TBA 810 S - fig. 13).

Fig. 12 - Maximum power dissipation versus ambient temperature (for TBA 810 AS only)

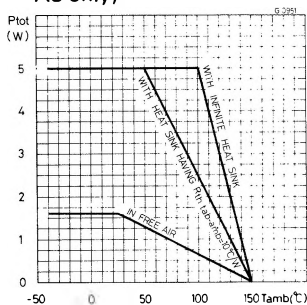
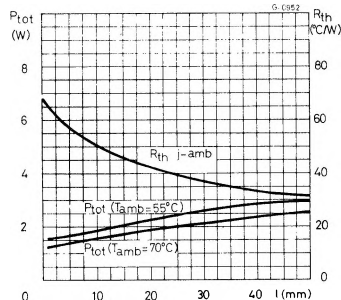
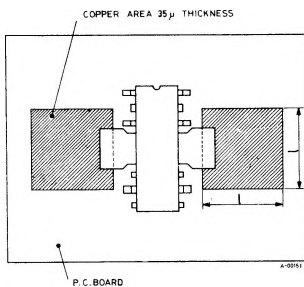


Fig. 13 - Maximum power dissipation versus copper area of the P.C. board (for TBA 810 S only)



During soldering the tabs temperature must not exceed 260°C and the soldering time must not be longer than 12 seconds.

Fig. 14a and 14b show two ways that can be used for mounting the device.

Fig. 14a shows a method of mounting the TBA 810 S, that is satisfactory both from the point of view of heat dissipation and from mechanical considerations. For TBA 810 AS the desired thermal resistance is obtained by fixing the elements shown in fig. 14b, to a suitably dimensioned plate. This plate can also act as a support for the whole printed circuit board; the mechanical stresses do not damage the integrated circuit. This is firmly fixed to the element, in fig. 14b.

Fig. 14a

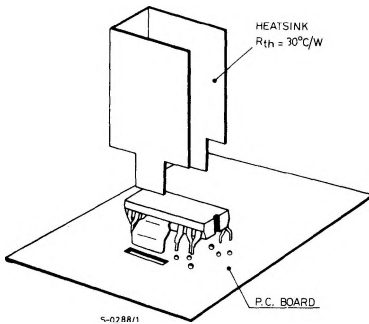
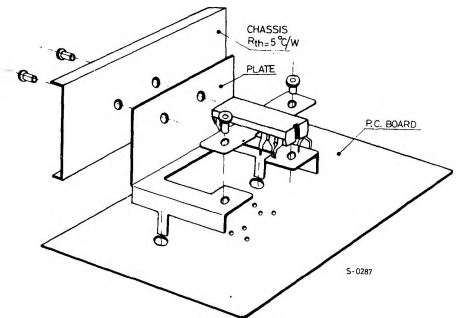


Fig. 14b



THERMAL SHUT-DOWN

The presence of a thermal limiting circuit offers the following advantages:

- 1) An overload on the output (even if it is permanent), or an above-limit ambient temperature can be easily supported.
- 2) The heat sink can have a smaller factor of safety compared with that of a conventional circuit. There is no device damage in the case of too high a junction temperature: all that happens is that P_o (and therefore P_{tot}) and I_d are reduced (fig. 15).

Fig. 15 - Output power and drain current versus package temperature

