

**INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP****SE/NE5532/5532A****DESCRIPTION**

The 5532 is a dual high-performance low noise operational amplifier. Compared to most of the standard operational amplifiers, such as the 1458, it shows better noise performance, improved output drive capability and considerably higher small-signal and power bandwidths.

This makes the device especially suitable for application in high quality and professional audio equipment, instrumentation and control circuits, and telephone channel amplifiers. The op amp is internally compensated for gains equal to one. If very low noise is of prime importance, it is recommended that the 5532A version be used which has guaranteed noise voltage specifications.

**ABSOLUTE MAXIMUM RATINGS**

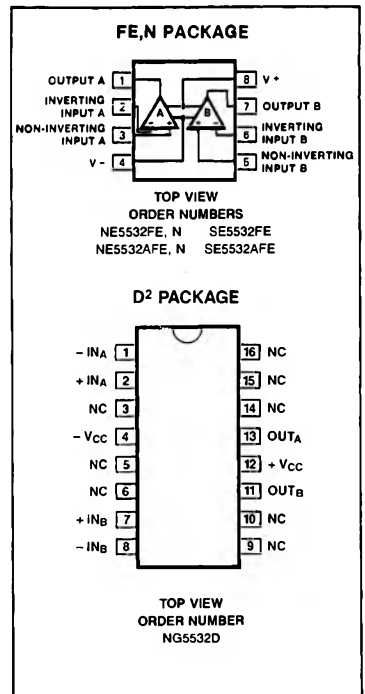
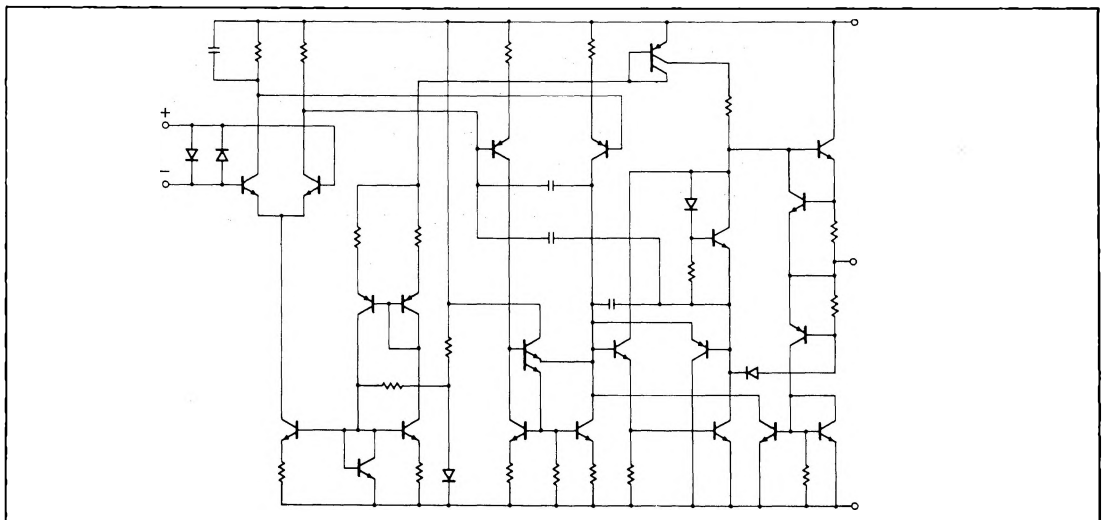
PARAMETER	RATING	UNIT
$V_S$ Supply voltage	$\pm 22$	V
$V_{IN}$ Input voltage	$\pm V$ supply	V
$V_{DIFF}$ Differential input voltage <sup>1</sup>	$\pm .5$	V
$T_A$ Operating temperature range		
NE5532/A	0 to 70	°C
SE5532/A	-55 to +125	°C
$T_{STG}$ Storage temperature	-65 to +150	°C
$T_J$ Junction temperature	150	°C
$P_D$ Power dissipation		
5532FE	1000	mW
Lead temperature (soldering, 10 sec)	300	°C

**NOTES:**

- Diodes protect the inputs against over-voltage. Therefore, unless current-limiting resistors are used, large currents will flow if the differential input voltage exceeds 0.6V. Maximum current should be limited to  $\pm 10$ mA.
- Thermal resistance of the FE package is 125°C/W.

**FEATURES**

- Small-signal bandwidth: 10MHz
- Output drive capability: 600 $\Omega$ , 10V (rms)
- Input noise voltage: 5nV/ $\sqrt{\text{Hz}}$  (typical)
- DC voltage gain: 50000
- AC voltage gain: 2200 at 10kHz
- Power bandwidth: 140kHz
- Slew-rate: 9V/ $\mu\text{s}$
- Large supply voltage range:  $\pm 3$  to  $\pm 20$ V
- Compensated for unity gain

**PIN CONFIGURATION****EQUIVALENT SCHEMATIC (EACH AMPLIFIER)**

## INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP

## SE/NE5532/5532A

DC ELECTRICAL CHARACTERISTICS  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{V}$  unless otherwise specified.<sup>1,2</sup>

PARAMETER	TEST CONDITIONS	SE5532/5532A			NE5532/5532A			UNIT
		Min	Typ	Max	Min	Typ	Max	
$V_{OS}$ Offset voltage	Over temperature		0.5	2		0.5	4	mV
$\Delta V_{OS}/\Delta T$			5	3		5	5	mV/ $\mu\text{V}/^\circ\text{C}$
$I_{OS}$ Offset current	Over temperature			100		10	150	nA
$\Delta I_{OS}/\Delta T$			200	200		200	200	nA/ pA/ $^\circ\text{C}$
$I_B$ Input current	Over temperature		200	400		200	800	nA
$\Delta I_B/\Delta T$			5	700		5	1000	nA/ mA/ $^\circ\text{C}$
$I_{CC}$ Supply current	Over temperature			13		8	16	mA
$V_{CM}$ Common mode input range								mA
CMRR Common mode rejection ratio		$\pm 12$	$\pm 13$		$\pm 12$	$\pm 13$		V
PSRR Power supply rejection ratio		80	100		70	100		dB
$A_{VOL}$ Large signal voltage gain	$R_L \geq 2\text{k}\Omega$ , $V_O = \pm 10\text{V}$ Over temperature $R_L \geq 600\Omega$ , $V_O = \pm 10\text{V}$ Over temperature	50			25	100		V/mV
		25			15			V/mV
		40			15	50		V/mV
		20			10			V/mV
$V_{OUT}$ Output swing	$R_L \geq 600\Omega$ Over temperature $R_L \geq 600\Omega$ , $V_S = \pm 18\text{V}$ Over temperature $R_L \geq 2\text{k}\Omega$ over temp.				$\pm 12$	$\pm 13$		V
					$\pm 10$	$\pm 12$		V
		$\pm 15$	$\pm 16$					V
					$\pm 12$	$\pm 14$		V
$R_{IN}$ Input resistance		30	300		30	300		k $\Omega$
$I_{SC}$ Output short circuit current		10	38	60	10	38	60	mA

AC ELECTRICAL CHARACTERISTICS  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{V}$  unless otherwise specified.

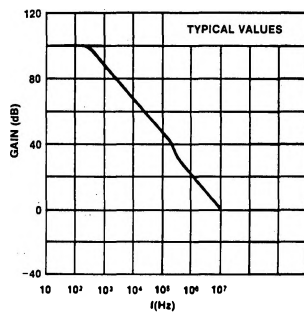
PARAMETER	TEST CONDITIONS	SE/NE5532/5532A			UNIT
		Min	Typ	Max	
$R_{OUT}$ Output resistance	$A_V = 30\text{dB}$ Closed loop $f = 10\text{kHz}$ , $R_L = 600\Omega$		0.3		$\Omega$
Overshoot	Voltage follower $V_{IN} = 100\text{mV}$ p-p $C_L = 100\text{pF}$ $R_L = 600\Omega$		10		%
Gain	$f = 10\text{kHz}$		2.2		V/mV
Gain bandwidth product	$C_L = 100\text{pF}$ $R_L = 600\Omega$		10		MHz
Slew rate			9		V/ $\mu\text{s}$
Power bandwidth	$V_{OUT} = \pm 10\text{V}$ $V_{OUT} = \pm 14\text{V}$ , $R_L = 600\Omega$ , $V_{CC} = \pm 18\text{V}$		140		kHz
			100		kHz

ELECTRICAL CHARACTERISTICS  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 15\text{V}$  unless otherwise specified.

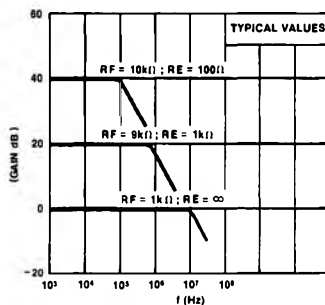
PARAMETER	TEST CONDITIONS	SE/NE5532			SE/NE5532A			UNIT
		Min	Typ	Max	Min	Typ	Max	
Input noise voltage	$f_o = 30\text{Hz}$		8			8	12	nV/ $\sqrt{\text{Hz}}$
	$f_o = 1\text{kHz}$		5			5	6	nV/ $\sqrt{\text{Hz}}$
Input noise current	$f_o = 30\text{Hz}$		2.7			2.7		pA/ $\sqrt{\text{Hz}}$
	$f_o = 1\text{kHz}$		0.7			0.7		pA/ $\sqrt{\text{Hz}}$
Channel separation	$f = 1\text{kHz}$ , $R_S = 5\text{k}\Omega$		110			110		dB

## TYPICAL PERFORMANCE CHARACTERISTICS

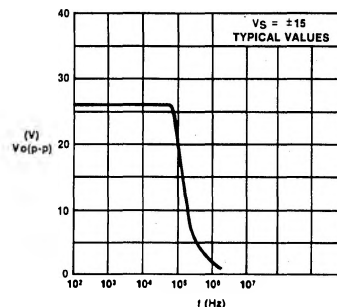
OPEN LOOP FREQUENCY RESPONSE



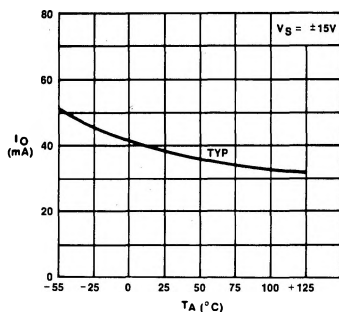
CLOSED LOOP FREQUENCY RESPONSE



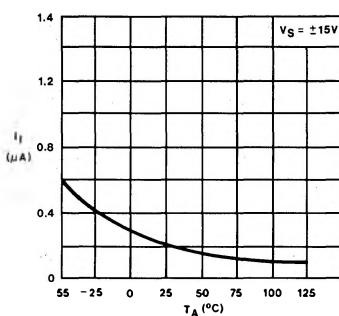
LARGE-SIGNAL FREQUENCY RESPONSE



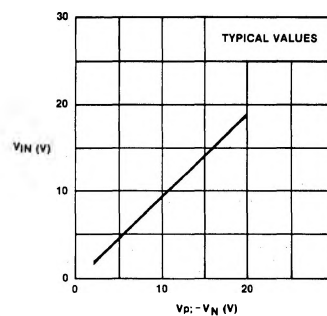
OUTPUT SHORT-CIRCUIT CURRENT



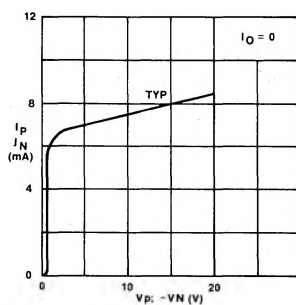
INPUT BIAS CURRENT



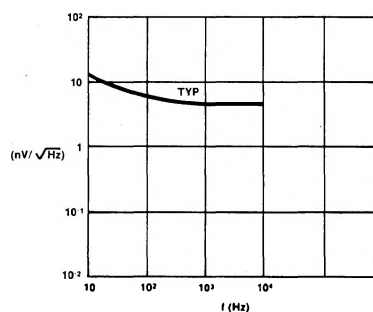
INPUT COMMON MODE VOLTAGE RANGE



SUPPLY CURRENT

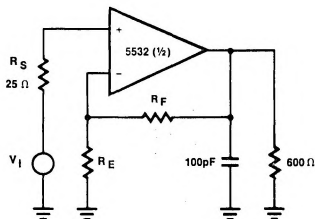


INPUT NOISE VOLTAGE DENSITY

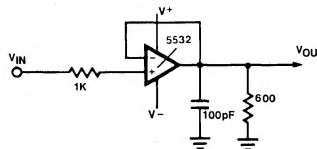


## TEST CIRCUITS

CLOSED LOOP FREQUENCY RESPONSE



VOLTAGE FOLLOWER



## AUDIO CIRCUITS USING THE NE5532/33/34

More detailed information is available in the communications section of this manual, regarding other audio circuits. The following will explain the Signetics line of low noise op amps and show their use in some audio applications.

## DESCRIPTION

The 5532 is a dual high-performance low noise operational amplifier. Compared to most of the standard operational amplifiers, such as the 1458, it shows better noise performance, improved output drive capability and considerably higher small-signal and power bandwidths.

This makes the device especially suitable for application in high quality and professional audio equipment, instrumentation and control circuits, and telephone channel amplifiers. The op amp is internally compensated for gains equal to one. If very low noise is of prime importance, it is recommended that the 5532A version be used which has guaranteed noise voltage specifications.

## APPLICATIONS

The Signetics 5532 High Performance Op Amp is an ideal amplifier for use in high quality and professional audio equipment which requires low noise and low distortion.

The circuit included in this application note has been assembled on a P.C. board, and tested with actual audio input devices (Tuner and Turntable). It consists of an RIAA pre-amp, input buffer, 5-band equalizer, and mixer. Although the circuit design is not new, its performance using the 5532 has been improved.

The RIAA pre-amp section is a standard compensation configuration with low frequency boost provided by the Magnetic cartridge and the RC network in the op amp feedback loop. Cartridge loading is accomplished via R1. 47k was chosen as a typical value, and may differ from cartridge to cartridge.

The Equalizer section consists of an input buffer, 5 active variable band pass/notch (depending on R9's setting) filters, and an output summing amplifier. The input buffer is a standard unity gain design providing impedance matching between the pre amplifiers and the equalizer section. Because the 5532 is internally compensated, no external compensation is required. The 5-band active filter section is actually 5 individual active filters with the same feedback design for all 5. The main difference in all five stages is the values of C5 and C6 which are responsible for setting the center frequency of each stage. Linear pots are recommended for R9. To simplify use of this circuit, a component value table is provided, which lists center frequencies and their associated capacitor values. Notice that C5 equals (10) C6, and that the Value of R8 and R10 are related to R9 by a factor of 10 as well. The values listed in the table are common and easily found standard values.

## RIAA EQUALIZATION AUDIO PREAMPLIFIER USING NE5532A

With the onset of new recording techniques along with sophisticated playback equipment, a new breed of low noise operational amplifiers was developed to complement the state-of-the-art in audio reproduction. The first ultra low noise op amp introduced by Signetics was called the NE5534A. This is a single operational amplifier with less

than 4nV/ $\sqrt{\text{Hz}}$  input noise voltage. The NE5534A is internally compensated at a gain of three. This device has been used in many audio preamp and equalizer (active filter) applications since its introduction early last year.

Many of the amplifiers that are being designed today are dc coupled. This means that very low frequencies (2-15Hz) are being amplified. These low frequencies are common to turntables because of rumble and tone arm resonances. Since the amplifiers can reproduce these sub-audible tones, they become quite objectionable because the speakers try to reproduce these tones. This causes non-linearities when the actual recorded material is amplified and converted to sound waves.

The RIAA has proposed a change in its standard playback response curve in order to alleviate some of the problems that were previously discussed. The changes occur primarily at the low frequency range with a slight modification to the high frequency range. (See Figure 2). Note that the response peak for the bass section of the playback curve now occurs at 31.5Hz and begins to roll off below that frequency. The rolloff occurs by introducing a fourth R/C network occurs by introducing a fourth R/C network with a 7950 $\mu\text{s}$  time constant to the three existing networks that make up the equalization circuit. The high end of the equalization curve is extended to 20kHz, because recordings at these frequencies are achievable on many current discs.

## NE5533/34 DESCRIPTION

The 5533/5534 are dual and single high-performance low noise operational amplifiers. Compared to other operational amplifiers



# INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP

SE/NE5532/5532A

## PROPOSED RIAA PLAYBACK EQUALIZATION

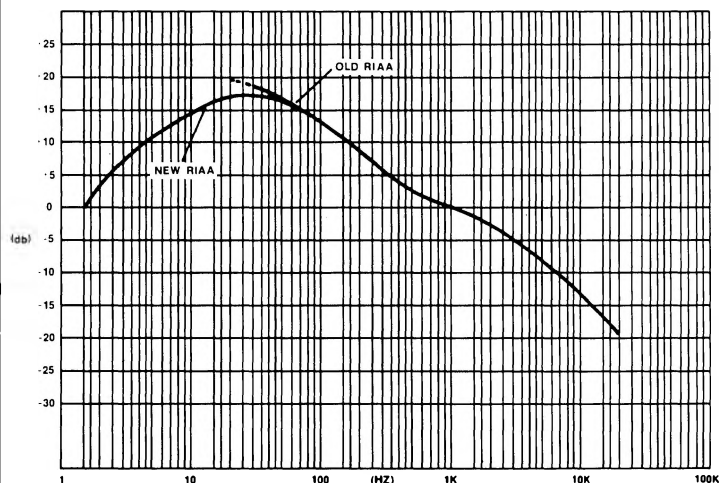
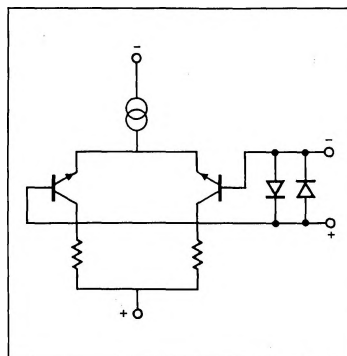


Figure 2



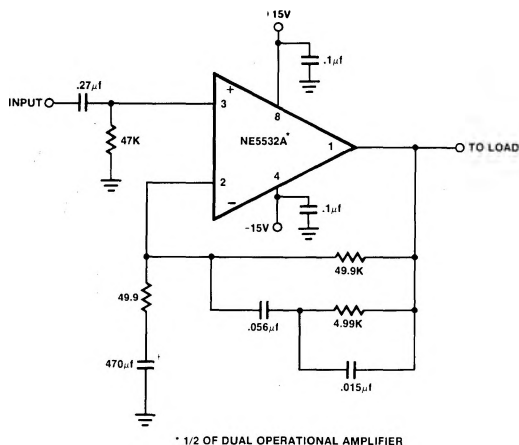
Consider the unity gain follower as an example:

Assume a signal input square wave with  $dV/dt$  of 250V per  $\mu s$  and 2V peak amplitude as shown. If a 22 pF compensation capacitor is inserted and the  $R_1, C_1$  circuit deleted, the device slew rate falls to approximately 7V/ $\mu s$ . The input waveform will reach 2V/250V/ $\mu s$  or 8 ns, while the output will have changed  $(8 \times 10^{-3})$  (7) only 56 mV. The differential input signal is then  $(V_{IN} - V_O) R_1 / R_1 + R_1$  or approximately 1V.

The diode limiter will definitely be active and output distortion will occur; therefore,  $V_{in} < 1V$  as indicated.

Next, a sine wave input is used with a similar circuit.

## RIAA PHONOGRAPH PREAMPLIFIER USING THE NE5532A

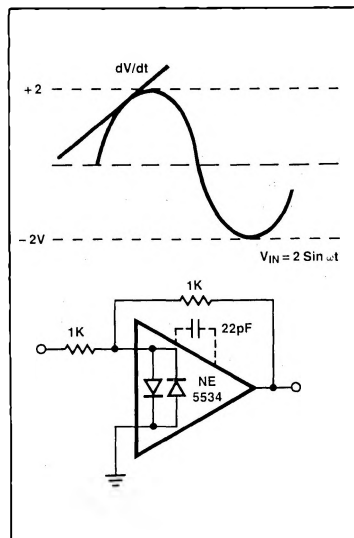


\* 1/2 OF DUAL OPERATIONAL AMPLIFIER

### NOTE

All resistors are 1% metal film and are valued in

Figure 3



# INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP SE/NE5532/5532A

The slew rate of the input waveform now depends on frequency and the exact expression is

$$\frac{dv}{dt} = 2\omega \cos \omega t$$

The upper limit before slew rate distortion occurs for *small signal* ( $V_{IN} < 100$  mV) conditions is found by setting the slew rate to  $7V/\mu s$ . That is:

$$7 \times 10^6 V/\mu s = 2\omega \cos \omega t$$

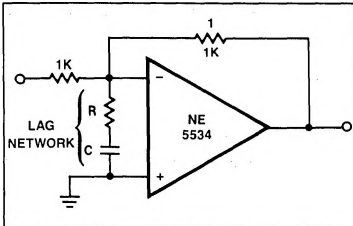
at  $\omega t = 0$

$$\omega_{LIMIT} = \frac{7 \times 10^6}{2} = 3.5 \times 10^6 \text{ rad/s}$$

$$f_{LIMIT} = \frac{3.5 \times 10^6}{2\pi} \approx 560 \text{ kHz}$$

## External Compensation Network Improves Bandwidth

By using an external lead-lag network, the follower circuit slew rate and small signal bandwidth can be increased. This may be useful in situations where a closed-loop gain less than 3 to 5 is indicated. A number of examples are shown in subsequent figures. The principle benefit of using the network approach is that the full slew rate and bandwidth of the device is retained, while impulse-related parameters such as damping and phase margin are controlled by choosing the appropriate circuit constants. For example, consider the following configuration:



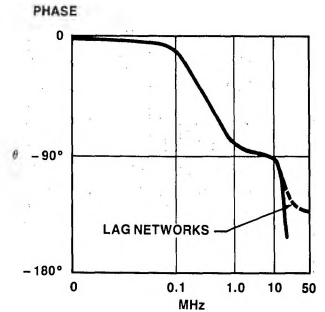
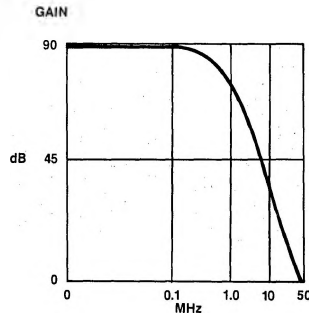
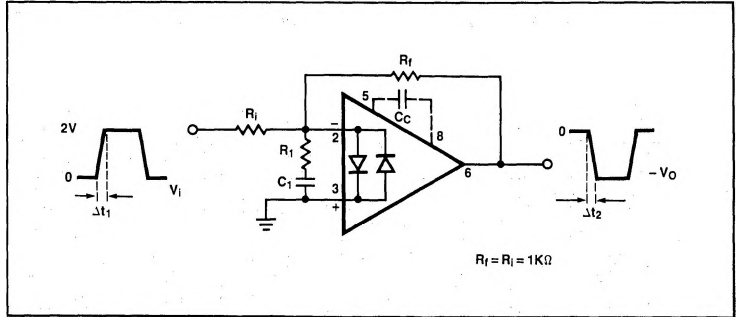
The major problem to be overcome is poor phase margin leading to instability.

By choosing the lag network break frequency one decade below the unity gain crossover frequency (30-50 MHz), the phase and gain margin are improved. An appropriate value for R is  $270\Omega$ . Setting the lag network break frequency at 5 MHz, C may be calculated

$$C = \frac{1}{2\pi \cdot 270 \cdot 5 \times 10^6}$$

118 = pF

A single pole and zero inserted in the transfer function will give an added  $45^\circ$  of phase margin depending on the network values.



## RULES AND EXAMPLES

### Compensation Using Pins 5 and 8 (Limited Bandwidth and Slew Rate)

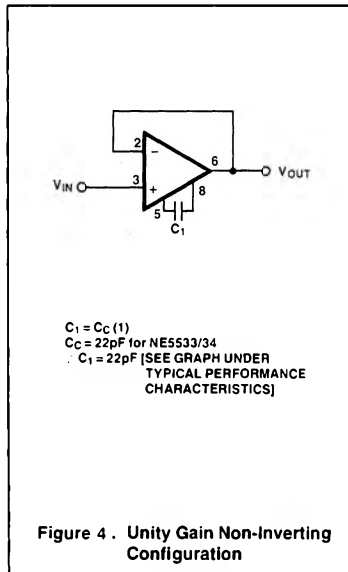


Figure 4. Unity Gain Non-Inverting Configuration

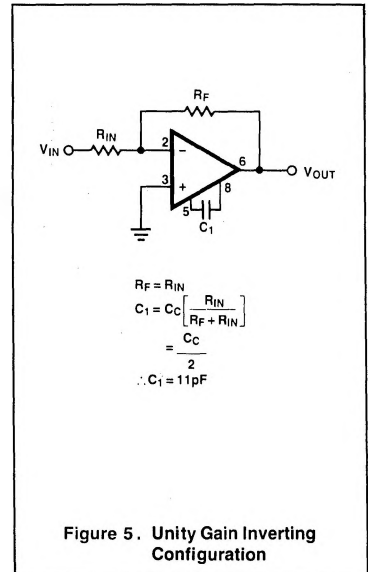


Figure 5. Unity Gain Inverting Configuration

# External Compensation for Wideband Voltage Follower

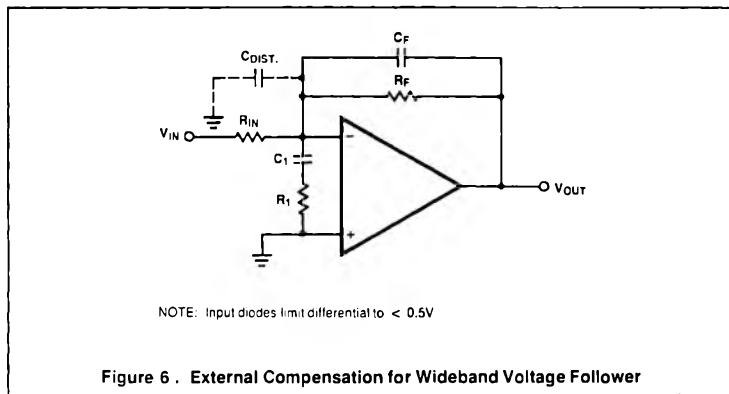


Figure 6 . External Compensation for Wideband Voltage Follower

## Calculating the Lead-Lag Network

$$C_1 = \frac{1}{2\pi F_1 R_1} \quad \text{Let } R_1 = \frac{R_{IN}}{10}$$

where  $F_1 = \frac{1}{10} (\text{UGBW})$

UGBW = 30 MHz

## Shunt Capacitance Compensation

$$C_F = \frac{1}{2\pi F_F R_F}, \quad F_F \approx 30 \text{ MHz}$$

or

$$C_F \approx \frac{C_{DIST}}{A_{CL}}$$

$C_{DIST} \approx \text{Distributed Capacitance} \approx 2\text{-}3\text{pF}$

Many audio circuits involve carefully tailored frequency responses. Pre-emphasis is used in all recording mediums to reduce noise and produce flat frequency response. The most often used de-emphasis curves for broadcast and home entertainment systems are shown in Figure 7. Operational amplifiers are well suited to these applications because of their high gain and easily tailored frequency response.

## 3.75 IPS TAPE EQUALIZATION

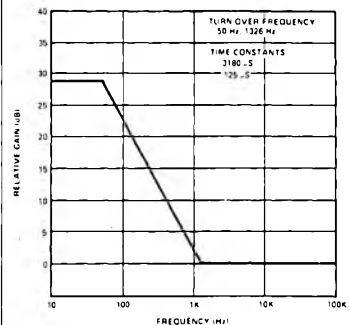


Figure 7c

## RIAA EQUALIZATION

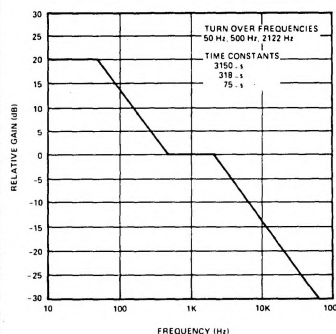


Figure 7a

## BASE TREBLE CONTROL CURVE

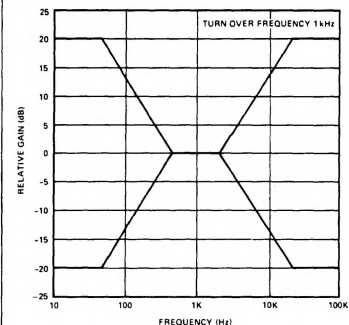


Figure 7d

## NAB STANDARD PLAYBACK 7 1/2 IPS

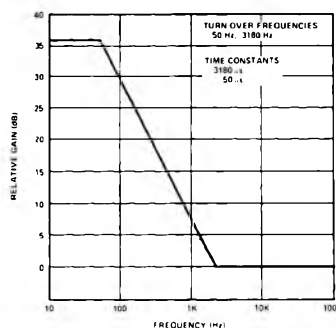


Figure 7b

## STANDARD FM BROADCAST EQUALIZATION

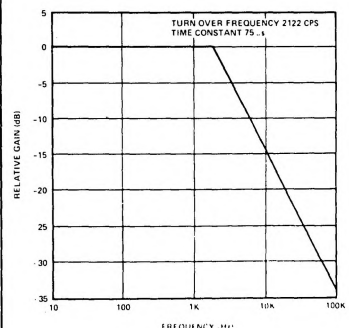


Figure 7e



# INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP SE/NE5532/5532A

## RIAA PREAMP USING THE NE5534

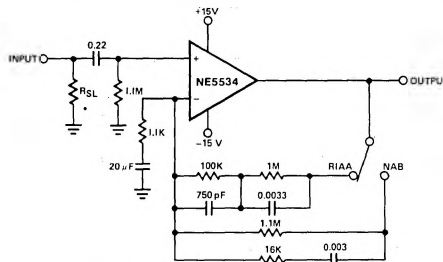
The preamplifier for phono equalization is shown in Figure 8 along with the theoretical and actual circuit response.

Low frequency boost is provided by the inductance of the magnetic cartridge with the RC network providing the necessary break points to approximate the theoretical RIAA curve.

## RUMBLE FILTER

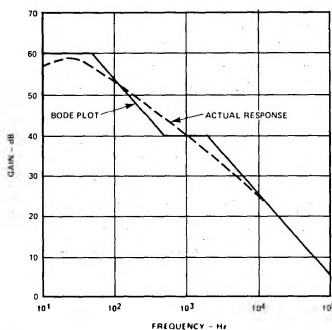
Following the amplifier stage, rumble and scratch filters are often used to improve overall quality. Such a filter designed with op amps uses the 2 pole Butterworth approach and features switchable break points. With the circuit of Figure 9 any degree of filtering from fairly sharp to none at all is switch selectable.

### PREAMPLIFIER—RIAA/NAB COMPENSATION



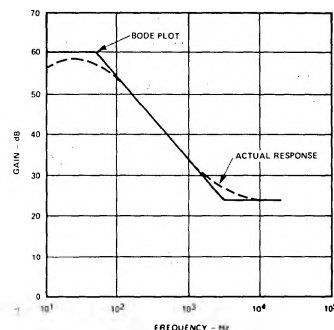
\*Select to provide specified transistor loading.  
Output Noise > 0.8mV rms (with input shorted)  
All resistor values are in ohms.

Figure 8a



Bode Plot of RIAA Equalization and the response realized in an actual circuit using the 531.

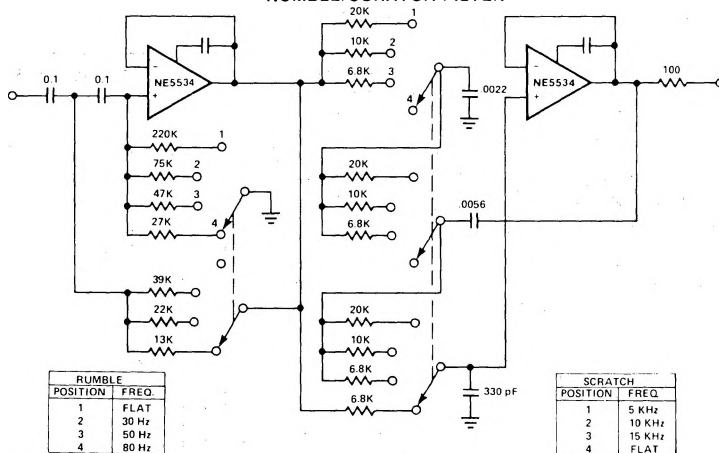
Figure 8b



Bode Plot of NAB Equalization and the response realized in an actual circuit using the 531.

Figure 8c

### RUMBLE/SCRATCH FILTER

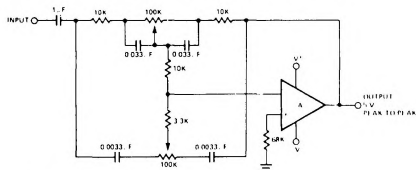


All resistor values are in ohms.

Figure 9

# INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP SE/NE5532/5532A

## TONE CONTROL CIRCUIT FOR OPERATIONAL AMPLIFIERS



All resistor values are in ohms.

### NOTES

1. Amplifier A may be a NE531 or 301. Frequency compensation, as for unity gain non-inverting amplifiers, must be used.
2. Turn-over frequency—1kHz.
3. Bass boost +20dB at 20Hz, bass cut -20dB at 20Hz, treble boost +19dB at 20kHz, treble cut -19dB at 20kHz.

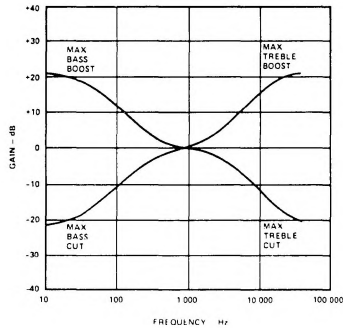


Figure 10

## TONE CONTROL

Tone control of audio systems involves altering the flat response in order to attain more low frequencies or more high ones dependent upon listener preference. The circuit of Figure 10 provides 20dB of bass or treble boost or cut as set by the variable resistance. The actual response of the circuit is shown also.

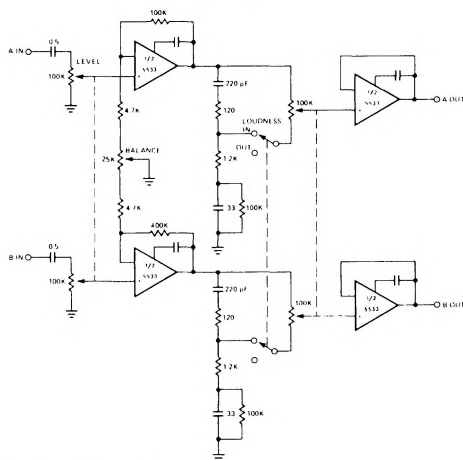
## BALANCE AND LOUDNESS AMPLIFIER

Figure 11 shows a combination of balance and loudness controls. Due to the non-linearity of the human hearing system the low frequencies must be boosted at low listening levels. Balance, level, and loudness controls provide all the listening controls to produce the desired music response.

## VOLTAGE AND CURRENT OFFSET ADJUSTMENTS

Many IC amplifiers include the necessary pin connections to provide external offset adjustments. Many times, however, it becomes necessary to select a device not possessing external adjustments. Figure 12, 13, and 14 suggest some possible arrangements for offset voltage adjust and bias current nulling circuitry. The circuitry of Figure 14 provides sufficient current into the input to cancel the bias current requirement. Although more simplified arrangements are possible the addition of Q2 and Q3 provide a fixed current level to Q1, thus, bias cancellation can be provided without regard to input voltage level.

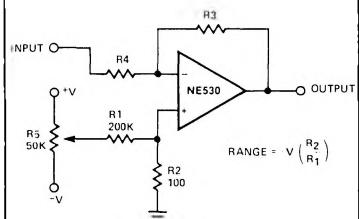
## BALANCE AMPLIFIER WITH LOUDNESS CONTROL



All resistor values are in ohms.

Figure 11

## UNIVERSAL OFFSET NULL FOR INVERTING AMPLIFIERS



All resistor values are in ohms.

Figure 12

# INTERNALLY COMPENSATED DUAL LOW NOISE OP AMP SE/NE5532/5532A

### UNIVERSAL OFFSET NULL FOR NONINVERTING AMPLIFIERS

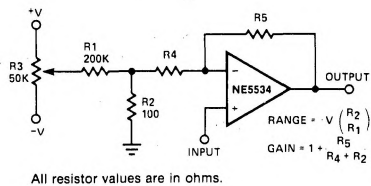


Figure 13

### BIAS CURRENT COMPENSATION

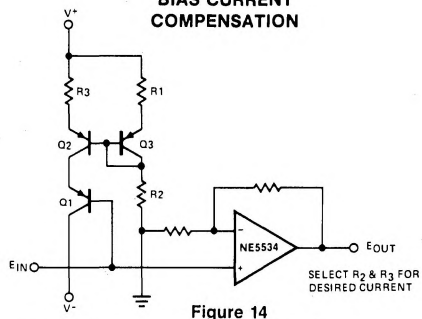


Figure 14

\*For additional information, consult the Applications Section.